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MIT Space Engineering Research Center

# INHIBITING MULTIPLE MODE VIBRATION IN

## CONTROLLED FLEXIBLE SYSTEMS

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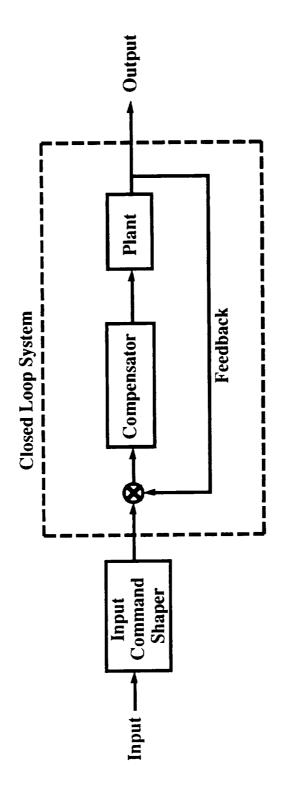
#### OUTLINE

Input Pre-Shaping Background

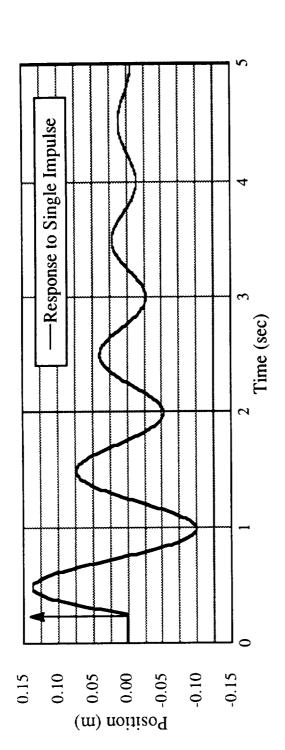
Developing Multiple-Mode Shapers

The MACE Test Article

Tests and Results



# LINEAR SYSTEM IMPULSE RESPONSE



$$y_i(t) = A_i e^{-\zeta} \omega (t - t_i) \sin((t - t_i) \omega \sqrt{1 - \zeta^2}$$

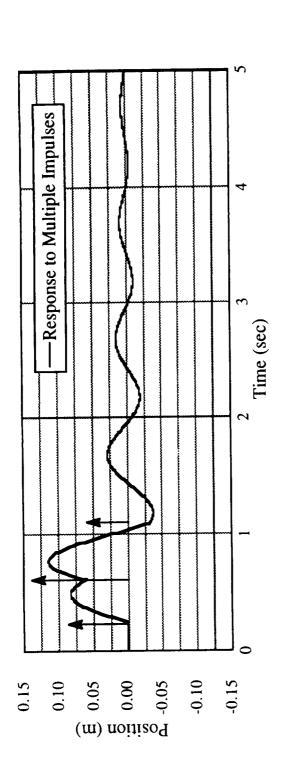
Magnitude of Impulse *i* Time of Impulse *i* Response to Impulse i yi Ai

System Natural Frequency  $3 \sim$ 

System Damping Ratio

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## RESPONSE TO "N" IMPULSES





i Impulse CounterNumber of Impulses

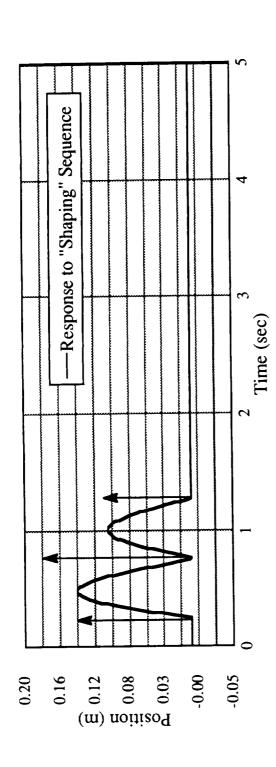
### AMPLITUDE OF THE MULTIPLE-IMPULSE RESPONSE ENVELOPE

$$Amp = \left[ \left( \sum_{i=1}^{N} A_i e^{-\zeta} \omega^{(t_N - t_i)} \sin(t_i \omega \sqrt{1 - \zeta^2}) \right)^2 + \right]$$

$$\left(\sum_{i=1}^{N} A_i e^{-\zeta} \omega^{(t_N - t_i)} \cos(t_i \omega \sqrt{1 - \zeta^2})\right)^2\right]^{I/2}$$

Expression for envelope amplitude at tw, the time of the final impulse.

# ELIMINATING RESIDUAL VIBRATION

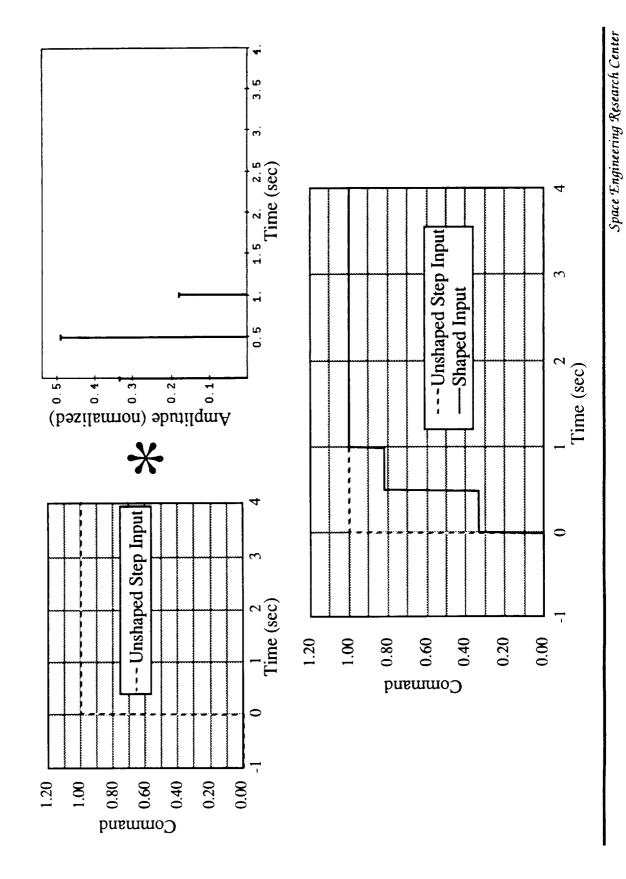


$$\sum_{i=1}^{N} A_i e^{-\zeta} \omega t_i \sin(t_i \omega \sqrt{1-\zeta^2}) = 0$$

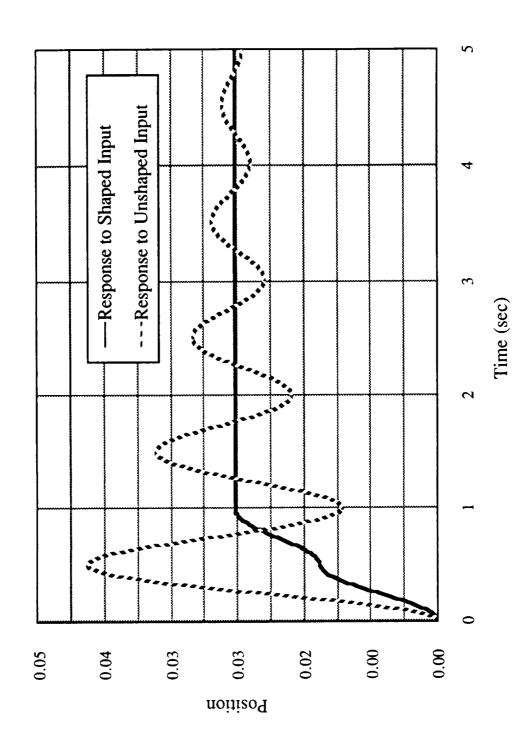
$$\sum_{i=1}^{N} A_i t_i e^{-\zeta} \omega t_i \sin(t_i \omega \sqrt{1-\zeta^2}) = 0$$

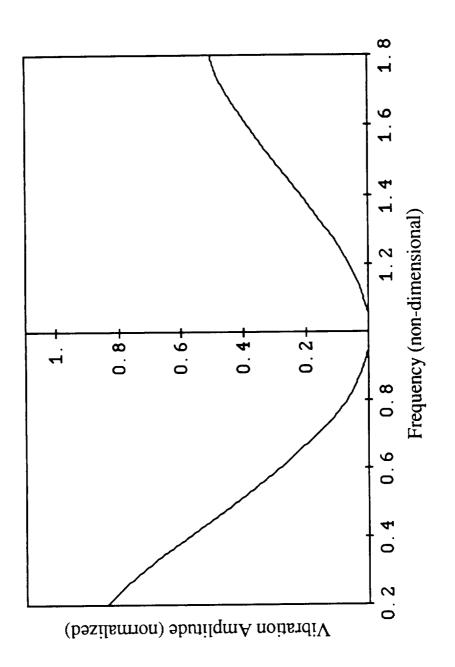
$$\sum_{i=1}^{N} A_i e^{-\zeta} \omega t_i \cos(t_i \omega \sqrt{1-\zeta^2}) = 0$$

$$\sum_{i=1}^{N} A_i t_i e^{-\zeta} \omega t_i \cos(t_i \omega \sqrt{1-\zeta^2}) = 0$$



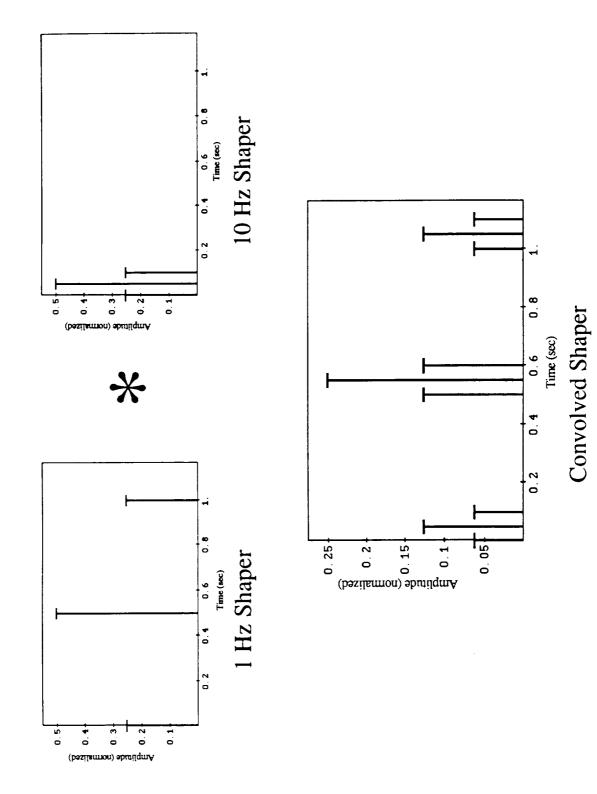
## RESPONSE TO INPUTS

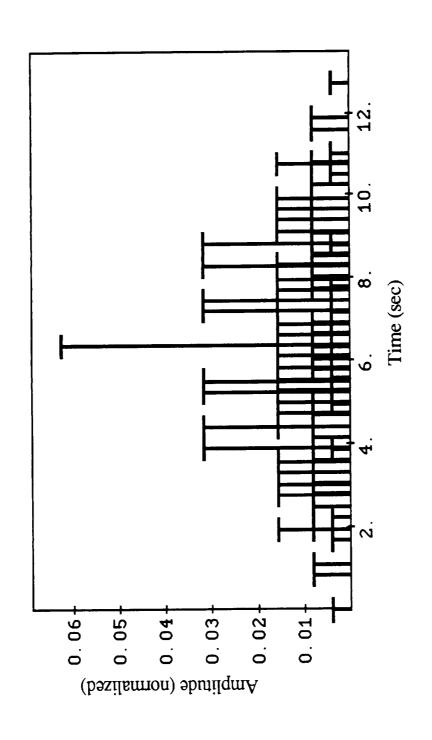




# EXTENDING TO MULTIPLE MODE PROBLEMS

### CONVOLUTION





$$\omega_1 = 0.20 \text{ Hz}$$
  $\omega_2 = 0.26 \text{ Hz}$ 

$$\omega_1 = 0.25 \text{ mz}$$
  $\omega_2 = 0.25 \text{ Hz}$   $\omega_3 = 0.45 \text{ Hz}$   $\omega_4 = 0.59 \text{ Hz}$ 

# DIRECT SOLUTION CONSTRAINT EQUATIONS

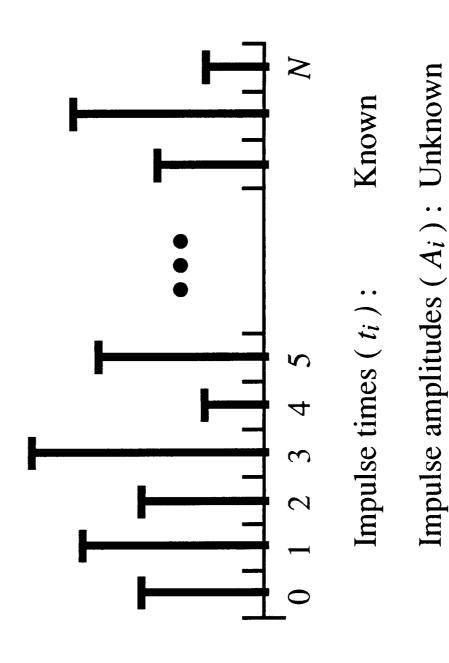
$$\sum_{1}^{N} A_{i} e^{-\zeta_{j}} \omega_{j} t_{i} \sin\left(t_{i} \omega_{j} \sqrt{1-\zeta_{j}^{2}}\right) = 0$$

$$\sum_{i=1}^{N} A_i e^{-\zeta_j \omega_j t_i} \cos(t_i \omega_j \sqrt{1-\zeta_j^2}) = 0$$

$$\sum_{i}^{N} A_{i} t_{i} e^{-\zeta_{j}} \omega_{j} t_{i} \sin(t_{i} \omega_{j} \sqrt{1 - \zeta_{j}^{2}}) = 0$$

$$\sum_{i=1}^{N} A_i t_i e^{-\zeta_j \omega_j t_i} \cos(t_i \omega_j \sqrt{1-\zeta_j^2}) = 0$$

These four equations are repeated for each mode "j"



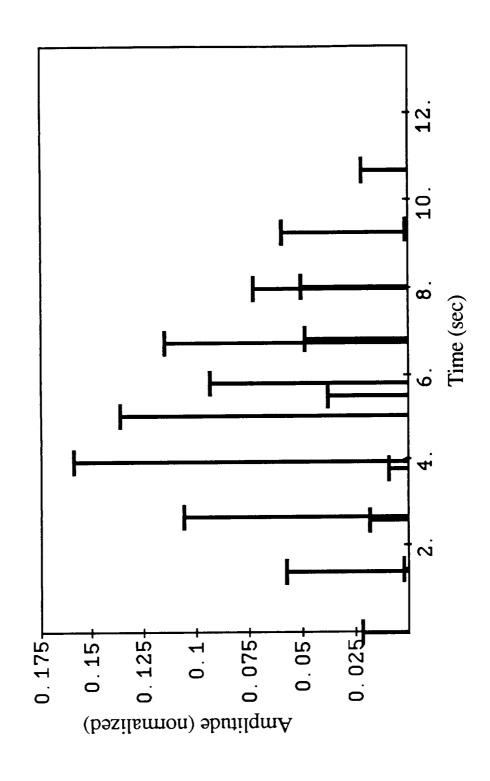
### COST FUNCTION

$$Cost = \sum_{j=1}^{M} \left[ \left( \sum_{i=1}^{N} A_i t_i^2 e^{-\zeta_j \omega_j t_i} \sin(t_i \omega_j \sqrt{1-\zeta_j^2}) \right)^2 \right]$$

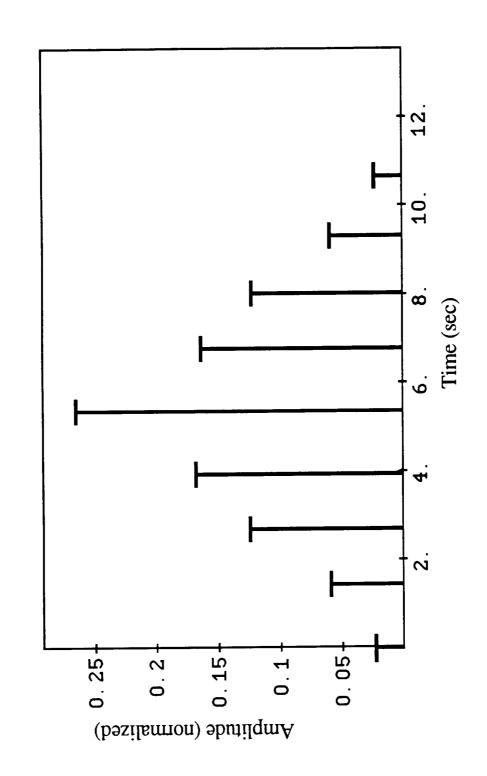
$$\left(\sum_{i=1}^{N} A_i t_i^2 e^{-\zeta_j \omega_j t_i} \cos\left(t_i \omega_j \sqrt{1-\zeta_j^2}\right)\right)^2\right]$$

M Number of modesj Modal index

# LINEAR APPROXIMATION SEQUENCE



## INTERPRETED LINEAR SEQUENCE



# EXACT DIRECT SOLUTION SEQUENCE

